Technical Article How to Get Started with Current Sense Amplifiers – Part 3



Daniel Harmon

In parts one and two of this series, I discussed concepts related to specifications of current-sense amplifiers and how to use the application requirements to narrow device selection. In this installment, I'll discuss how the current range helps derive the shunt-resistor value, as well as how the current range and shunt value combined with device performance drive a trade-off between accuracy and power dissipation.

Until the recent release of TI's INA250 current-sense amplifier (more on this later), the current didn't actually pass through the current-sense amplifier. Therefore, the current range being measured didn't directly dictate the device specifications.

For an analog output current-sense amplifier, the maximum current range combined with the full-scale input (maximum differential input voltage) will derive the ideal shunt resistor value, as shown in Equation 1:

$$R_{SHUNT} = V_{DIFF MAX} / I_{MAX}$$

(1)

If you look at most current-shunt monitor data sheets, you'll notice that the maximum differential voltage isn't specified; rather, a maximum output voltage swing is specified. You'll want to match this to the full-scale input range of the next link in the signal chain. To maximize performance, you'll want the maximum-output voltage swing to be greater than the next link's full-scale input range. Typically, the maximum output swing is a function of the supply voltage supplied to the current-sense amplifier. For example, with the INA282, the output-swing range is defined as 0.4V below the supply voltage to 0.04V above the voltage on the ground pin, as shown on page 6 of the datasheet.

At $T_A = 25^{\circ}$ C, V+ = 5 V, $V_{+IN} = 12$ V, $V_{REF1} = V_{REF2} = 2.048$ V referenced to GND, and $V_{SENSE} = V_{+IN} - V_{-IN}$ (unless otherwise noted)

PARAMETER	TEST CONDITIONS	MIN	ТҮР	MAX	UNIT	
VOLTAGE OUTPUT ⁽⁶⁾						
Swing to V+ power-supply rail	V+ = 5 V, R _{LOAD} = 10 kΩ to GND, T _A = -40°C to +125°C		(V+) – 0.17	(V+) – 0.4	V	
Swing to GND	R_{LOAD} = 10 kΩ to GND, T _A = -40°C to +125°C	(GND + 0.015	GND + 0.04	V	

(6) See typical characteristic graphs Figure 16 through Figure 18.

Figure 1. Electrical Characteristics of the INA82 Current-sense Amplifier

If you use the full-scale input range as the desired output swing of the current-shunt amplifier with maximum current flow, then you can modify the shunt-resistor equation, taking into account the gain (G_{AMP}) of the current-sense amplifier. Equation 2 shows this modification.

$$R_{SHUNT} = \frac{V_{Full \ Scale \ Input}}{I_{MAX} \times G_{AMP}}$$

(2)

1

Let's look at two examples of how to use this equation. For both examples, we will use the maximum current as 5A and the full-scale input of the next link in the signal chain as 2.5V. Let's consider using either the INA286 (gain of 100V/V) or INA284 (gain of 500V/V).



(3)

Device	Gain (V/V)	Ideal R _{sнимт} (ohms)
INA286	100	0.005
INA284	500	0.001

Figure 2. INA286 and INA284 gain and ideal R_{SHUNT} value with a maximum current of 5A and a full-scale input of 2.5V

The ideal R_{SHUNT} value may not be readily available, so you may have to choose the closest value – which may be is less than ideal. The reason you need to choose a resistor that is of a lesser ohmic value than the ideal is to keep the voltage input to the next link below the full-scale input level.

Using Equation 3, you will also need to verify that the minimum current value creates an output voltage from the current-shunt amplifier that is above the minimum output voltage.

$$V_{OUTMIN} \le I_{MIN} \times R_{SHUNT} \times G_{AMP}$$

Looking back at these two examples, you can calculate the minimum current for each solution as 80mA.

The next question is what to do with the fact that I have just calculated multiple options for different combinations of shunt value and amplifier gain. The answer comes down to a trade-off between the desired accuracy of the application versus the power dissipated in the shunt resistor. While I have not delved into accuracy yet, I will cover this in part 4 of this series; briefly, the larger the value of R_{SHUNT} , the higher the accuracy. However, as shown in Figure 3, the higher values of R_{SHUNT} lead to an increase in the power dissipated by the shunt resistor and adds to the overall load of the system.

Device	Gain (V/V)	R _{sнunt} (ohms)	V os (μV)	5A shunt power dissipation (W)	5A V _{os} error
INA286	100	0.005	70	0.125	0.28%
INA284	500	0.001	70	0.025	1.40%



You'll need to look at various current-sense amplifier options for gain and offset voltage and calculate how those options combined with the current range will affect the shunt-resistor value, achievable accuracy and power dissipation.

Most digital-output devices, such as the INA226, specify a full-scale shunt-voltage input range. This simplifies the calculations in many cases because there is not an additional gain stage to trade off against. The shunt value is simply the closest-available value resistor found by dividing the device's maximum-input voltage by the maximum current.

I mentioned briefly the brand-new INA250 current-sense amplifier. By integrating the shunt resistor, the INA250 can support a maximum current level based on the heat generated by the current flowing through the shunt. Look for more information in future blog posts about how the INA250 is redefining precision current measurement.

In the next installment, I will address the basics of accuracy and how device selection affects accuracy.

Additional Resources

- Learn more about TI's broad current-sense portfolio.
- Watch this video about how the INA300 is optimizing overcurrent detection.



- Learn from online training about getting started with current-sense amplifiers.
- Check out these related TI Designs reference designs:
 - High-Voltage 12V-400V DC Current-Sense Reference Design.
 - Current-Shunt Monitor with Transient Robustness Reference Design.
 - EMC-Compliant High-Side Current-Sensing Reference Design with Overvoltage Protection.

IMPORTANT NOTICE AND DISCLAIMER

TI PROVIDES TECHNICAL AND RELIABILITY DATA (INCLUDING DATA SHEETS), DESIGN RESOURCES (INCLUDING REFERENCE DESIGNS), APPLICATION OR OTHER DESIGN ADVICE, WEB TOOLS, SAFETY INFORMATION, AND OTHER RESOURCES "AS IS" AND WITH ALL FAULTS, AND DISCLAIMS ALL WARRANTIES, EXPRESS AND IMPLIED, INCLUDING WITHOUT LIMITATION ANY IMPLIED WARRANTIES OF MERCHANTABILITY, FITNESS FOR A PARTICULAR PURPOSE OR NON-INFRINGEMENT OF THIRD PARTY INTELLECTUAL PROPERTY RIGHTS.

These resources are intended for skilled developers designing with TI products. You are solely responsible for (1) selecting the appropriate TI products for your application, (2) designing, validating and testing your application, and (3) ensuring your application meets applicable standards, and any other safety, security, regulatory or other requirements.

These resources are subject to change without notice. TI grants you permission to use these resources only for development of an application that uses the TI products described in the resource. Other reproduction and display of these resources is prohibited. No license is granted to any other TI intellectual property right or to any third party intellectual property right. TI disclaims responsibility for, and you will fully indemnify TI and its representatives against, any claims, damages, costs, losses, and liabilities arising out of your use of these resources.

TI's products are provided subject to TI's Terms of Sale or other applicable terms available either on ti.com or provided in conjunction with such TI products. TI's provision of these resources does not expand or otherwise alter TI's applicable warranties or warranty disclaimers for TI products.

TI objects to and rejects any additional or different terms you may have proposed.

Mailing Address: Texas Instruments, Post Office Box 655303, Dallas, Texas 75265 Copyright © 2023, Texas Instruments Incorporated